

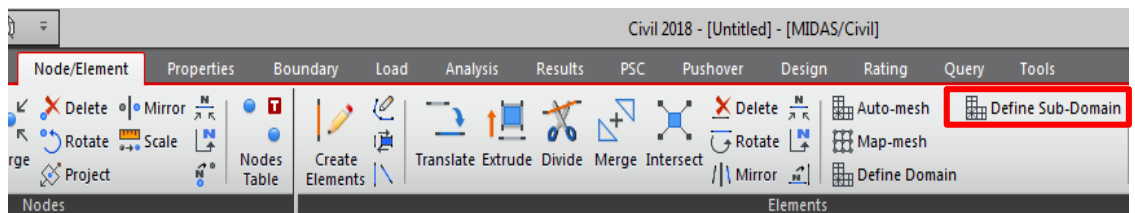
How can we design Beam(Slab) or Column(Wall) using plate element?



Plate Design is divided into Plate Beam (Slab) design and Plate Column (Wall) design, and the existing Beam / Column design is applied (as per AASHTO LRFD 12) to the plate elements modeled by the user. The design is carried out in sub-domain units. The maximum positive/negative moment and shear force are calculated by the concrete load combination for the elements defined in specific sub-domain.

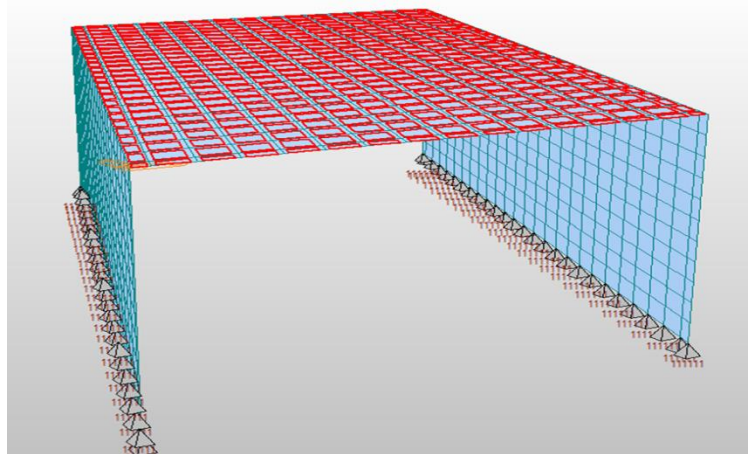
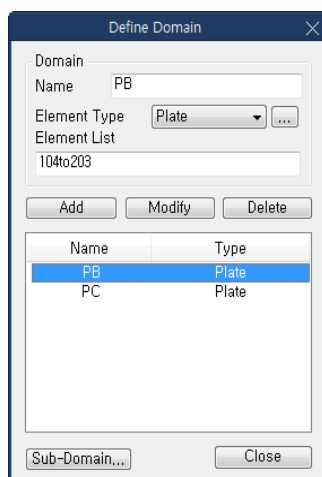
In Plate Design (AASHTO-LRFD12) design, thickness is used as the height and the width if used as unit width to perform design. Therefore, the strength and serviceability check results are represent the result from thickness and unit width. The main rebar and shear reinforcement are also converted into the reinforcement required to the unit width

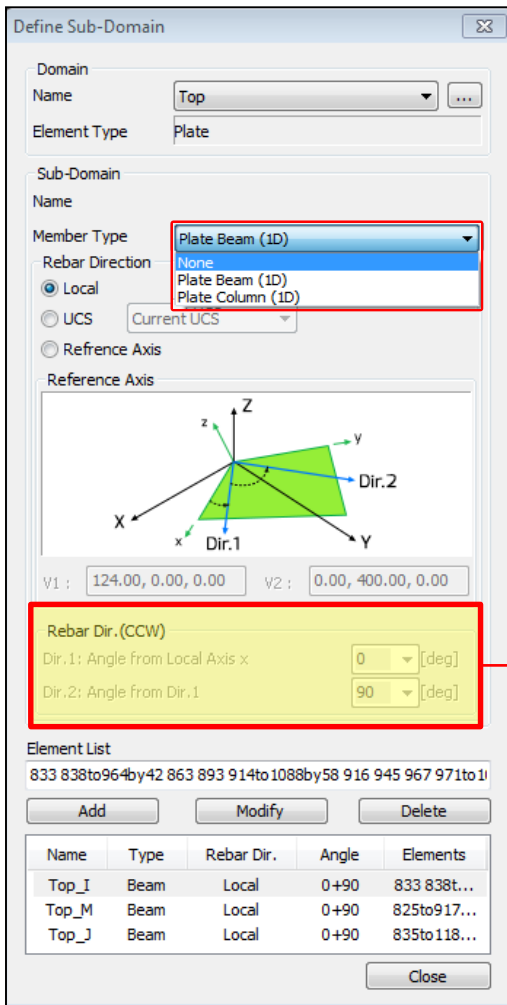
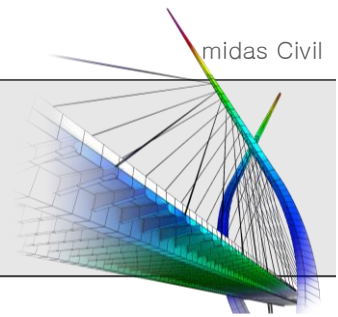
1. Define Domain



Node/Element > Elements > Define Domain/Sub-Domain

Pre / Post Processing Input Data for Plate Beam Design should be defined. After creating the plate element, Domain and Sub-Domain of specific elements should be defined and then Plate Member is assigned.





2. Define Sub-Domain

► Sub-Domain

Plate Design carries out design in designated sub-domain unit. Member Type is Plate Beam (1D), Plate Column (1D), and it is classified by selecting corresponding Member Type.

- Plate Beam (1D): Select this if you want Slab Design like 1 way Beam.
- Plate Column (1D): Select the Abutment/Side Wall Design like column under only axial force.

► Rebar Direction

Enter the direction of the rebar.

- **Local** : Use the local coordinate system of the plate element to define the rebar direction

Dir.1 : Local x-axis

Dir.2 : Local y-axis

- **UCS** : Select a predefined user coordinate system to define the rebar direction. If no user coordinate system is specified, the global coordinate system is used(Current UCS)

Dir.1 : UCS X-axis

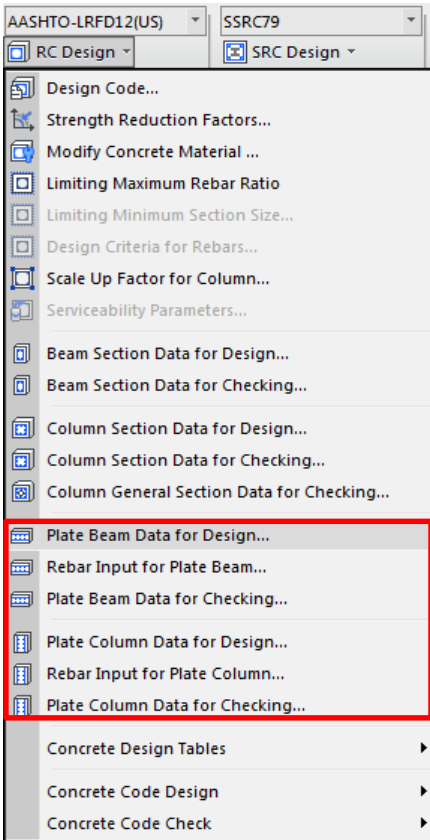
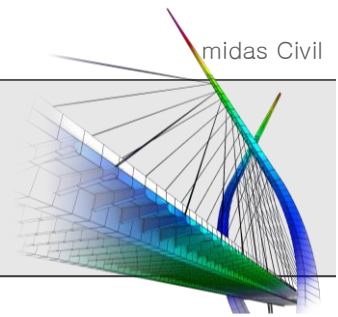
Dir.2 : UCS Y-axis

- **Reference Axis** : The user uses the coordinates defined by Reference Axis directly. Select V1 vector to define reference x-axis and select V2 vector to define the plane.

Dir.1 : Reference x-axis (V1)

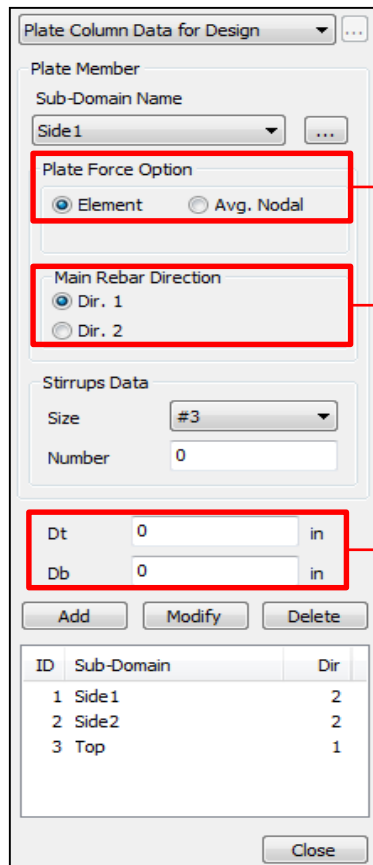
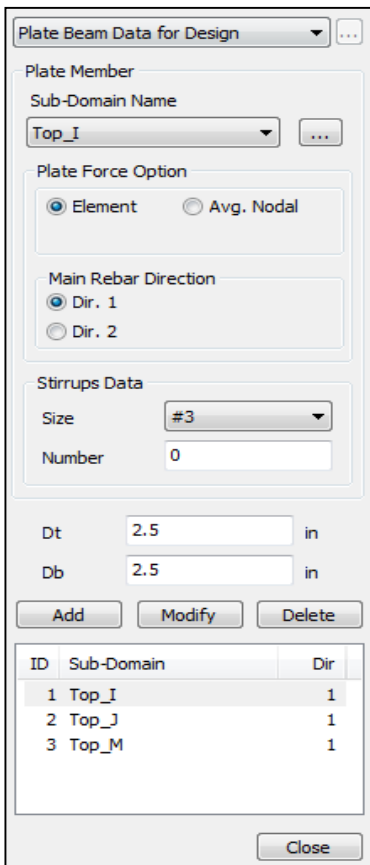
Dir.2 : 90 degree from Reference x-axis

*** Note : This feature is used for the calculation of Wood-Armer moment of specific direction. This will be fixed to default for Plate Design (Dir.1 = 0 deg, Dir.2 = 90 deg).**



2. Plate Beam / Column Design

- ▶ Plate Beam Data for Design ...
 - This Enter the data required for Plate Column Design.
- ▶ Rebar Input for Plate Beam...
 - Enter the reinforcement pattern to be applied in Beam Checking.
- ▶ Plate Beam Data for Checking...
 - Enter the data required for Plate Beam Checking
- ▶ Plate Column Data for Design...
 - Enter the data required for Plate Column Design.
- ▶ Rebar Input for Plate Column...
 - Enter the reinforcement pattern to be applied in Column Checking.
- ▶ Plate Column Data for Checking...
 - Enter the data required for Plate Column Checking



Element:

Display the contour using the internal forces calculated at each node of a n element.

Avg. Nodal:

Display the contour using the average internal nodal forces of the contiguous elements within the same Sub-Domain sharing the common nodes.

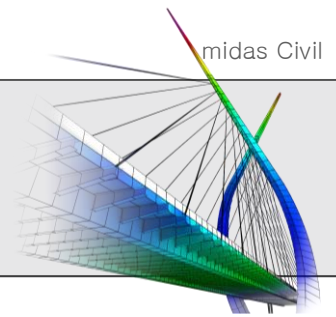
Define main rebar direction according to the direction defined at Sub-Domain

Cover Thickness of top and bottom



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Plate Beam Design Result Dialog

Code : AASHTO-LRFD12 Unit : kips , in , / in **Member forces are shown in terms of unit length**

Sub-Domain	SEL	Major Dir	CHK	Pos	Req_As	Elem.	Node	LCB_M	Mu	Mr	Ratio_M	Elem.	Node	LCB_V	Vu	Vr
Top_I	<input type="checkbox"/>	Dir1	OK	Pos	0.0181	833	C	1	0.00000	7.19464	0.0000	863	C	3	0.54797	1.1304
				Neg	0.0792	1020	1464	3	28.7453	29.6082	0.9709					
Top_J	<input type="checkbox"/>	Dir1	OK	Pos	0.0226	927	1443	4	8.64613	8.89366	0.9722	1194	1574	3	0.53053	1.1481
				Neg	0.0859	907	1439	3	31.2120	31.9761	0.9761					
Top_M	<input type="checkbox"/>	Dir1	OK	Pos	0.0370	989	1445	4	14.0982	14.4045	0.9787	1007	1506	4	0.36797	1.0171
				Neg	0.0181	825	C	1	0.00000	7.19464	0.0000					

Connect Model View

 C:\Users\Wnisk0201\Desktop
 Result View Option: All OK NG

The most critical position of the element is decided according to the largest amount of Reinforcement required (Req_As).

1. Design Condition

Design Type: Plate Beam (1D)
 Sub-Domain: Top_I
 Design Code: AASHTO-LRFD12
 Unit System: kips, in, /in
 Material Data: fc = 5, fy = 60, fys = 60 ksi
 Thickness: 10 in

2. Section Diagram

Element No: 833

Rebar Pattern: Top Required Rebar Area = 0.079249 in²
 Bot Required Rebar Area = 0.0181318 in²
 Required Stirrups Spacing: No Stirrup

3. Bending Moment Capacity

	Top(Negative)	Bottom(Positive)
Mu	28.75	0.00
Element No.	1020	833
Load Combination	S4_EHmax	S1_EHmax
Mr	29.61	7.19
Check Ratio (Mu/Mr)	0.9709	0.0000

4. Shear Capacity

Element No: 863
 Load Combination: S4_EHmax
 Applied Shear Strength: Vu = -0.5480
 Shear Strength (Out of plane): Vr = 1.13064
 Required Stirrups Spacing: 5.97188 in
 Shear Ratio: Vu/Vr = -0.5480 / 1.13064 = 0.485 < 1.000 0.K

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MIDAS (Modeling, Integrated Design & Analysis Software)
MIDAS/Civil - Design & checking system for windows
RC-Plate Member (Plate Beam/Column) Analysis and Design
Based On: AASHTO-LRFD12
(c) SINCE 1989
MIDAS Information Technology Co., Ltd. (MIDAS IT)
MIDAS IT Design Development Team
HomePage: www.MidasUser.com
MIDAS/Civil Version 8.6.5
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*.DEFINITION OF LOAD COMBINATIONS WITH SCALING UP FACTORS.

LCB	C	Loadcase Name(Factor)	+ Loadcase Name(Factor)	+ Loadcase Name(Factor)
1	1	SW(1.250) +	EV(1.300) +	EH(1.350)
2	1	SW(1.250) +	EV(1.300) +	EH(0.900)
3	1	SW(1.500) +	EV(1.300) +	EH(1.350)
4	1	SW(1.500) +	EV(1.300) +	EH(0.900)

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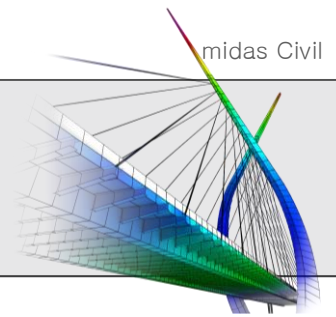
*.MIDAS/Civil - RC- PLATE BEAM Analysis/Design Program.
*.PROJECT :
*.DESIGN CODE : AASHTO-LRFD12, *.UNIT SYSTEM : kips, in, /in
*.SUB-DOMAIN : Top_I, Member Type = PLATE BEAM(1D), Dir = 1 )
*.DESCRIPTION OF PLATE BEAM DATA :
Thickness = 10.000 in.
Unit Width = 1 in.
Concrete Strength (fc) = 5,000 ksi.
Main Rebar Strength (fy) = 60,000 ksi.
Stirrups Strength (fys) = 60,000 ksi.
Modulus of Elasticity (Es) = 29000.000 ksi.
< Selected Elements >
All Elements
< Positive Bending Moment >
P-Mu = 0.00 in-kips/in., ELEM = 833, LCB = 1, NODE = Center
< Negative Bending Moment >
N-Mu = 28.75 in-kips/in., ELEM = 1020, LCB = 3, NODE = 1464
< Shear Force >
Vu = -0.55 kips/in., ELEM = 863, LCB = 3, NODE = Center
*.REINFORCEMENT PATTERN :
Dt = 2.500 { in. }
Db = 2.500 { in. }
Stirrups : No BarNum
  
```

[[[(*]]] ANALYZE POSITIVE BENDING MOMENT CAPACITY.

```

( ). Compute parameter.
-. phi = 0.90
-. Alpha = 0.85
-. Beta = 0.80
-. d = 7.5000 in.
-. ecu = 0.0030
  
```

Graphic and Detail Report of Design Result



Rebar Input for Plate Beam

Name: Top_I

Main Rebar | Distribution Bar

Num CTC

Top

As: 3.16 in²/ft Layer: 1

Layer	CTC	Size1	Size2	Dt
1	3	#8		2.5

Bottom

As: 3.16 in²/ft Layer: 1

Layer	CTC	Size1	Size2	Db
1	3	#8		2.5

Stirrup

Size: #3

Spacing: 0 in

Number: 0

Add Modify Delete

ID	Name
1	Top_I
2	Top_M
3	Top_J

Close

3. Plate Beam / Column Checking

► Main Rebar/Distribution Bar

The rebar can be inputted with either the number of rebar (Num) or spacing of rebar(CTC).

*** Note : Distribution bar data must be inputted to create Rebar input data.**

The area of reinforcement (As) is expressed in terms of unit length and this is fixed as unit ft or unit m depending on which unit system is chosen by the user.

Plate Checking result shows the same member force results using the area of reinforcement inputted by the user. The only difference is that axial force result is shown in Plate Column Checking.

The main target of this function is culvert and abutment. Axial force is not critical when we are designing culvert or abutment. Therefore this feature does not consider the benefit of axial force in calculation of flexural strength. However the calculation of axial resistance is provided in checking mode.

Plate Column Check Result Dialog

Code : AASHTO-LRFD12 Unit : kips , in , / in

Results : Strength Serviceability

Sub-Do main	SEL	Major Dir	CHK	Pos	Use_As	Elem.	Node	LCB_M	Mu	Mr	Ratio_M	Elem.	Node	LCB_P	Pu	Pr
Side1		Dir1	NG	Pos	0.0658	1721	1484	3	27.8226	24.9417	1.1155	1743	1484	3	1.51011	37.381
				Neg	0.0658	1944	1950	3	21.3409	24.9417	0.8556					

Connect Model View

Select All Unselect All Re-calculation

Detail... C:\Users\Wnks0201\W\Desktop\ ... <<

Graphic... Close

Result View Option

All OK NG

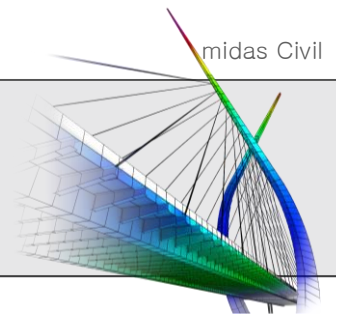
Copy Table

Graphic and Detail Report of Design Result

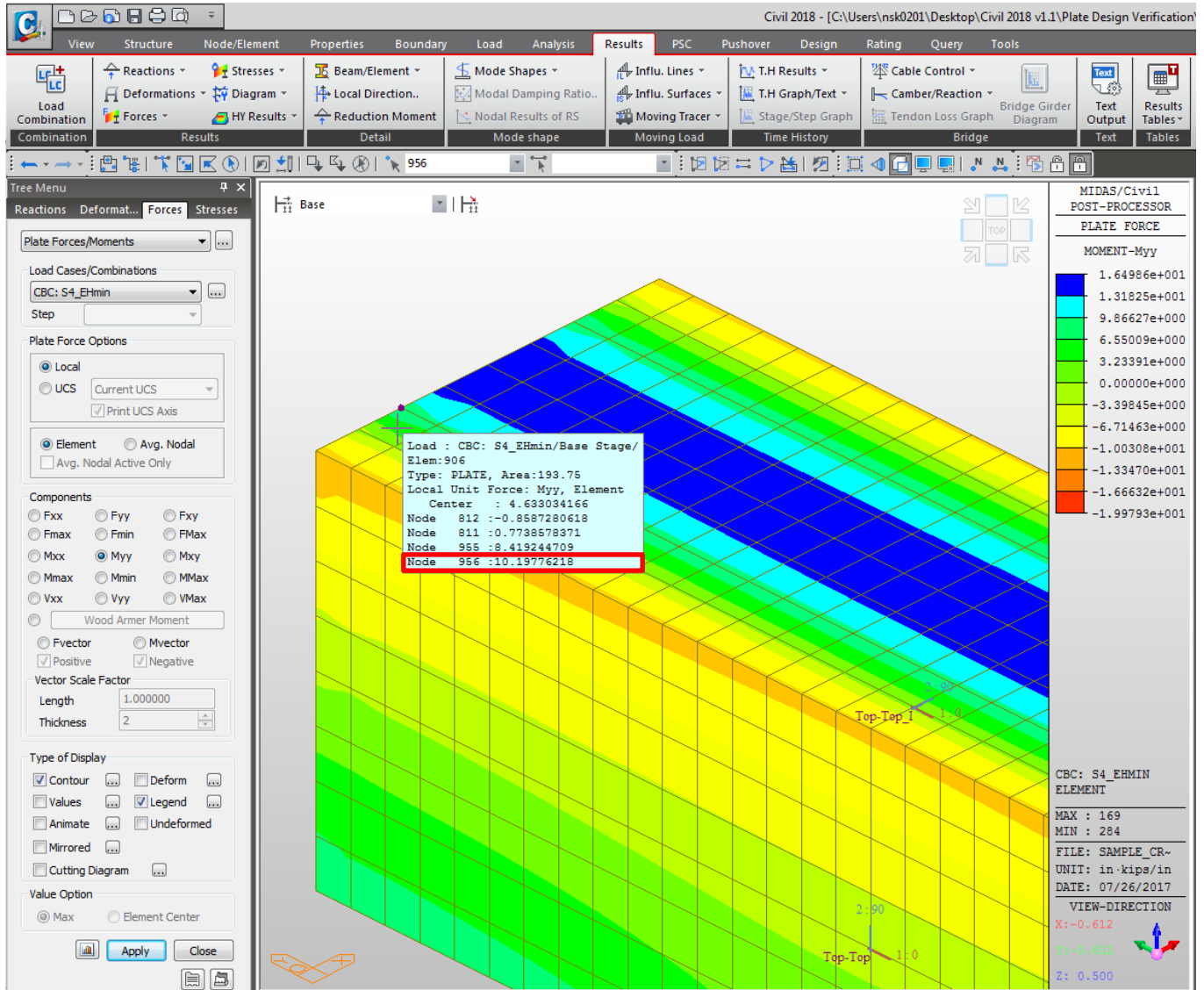


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Design result can be double checked with the analysis result. The detail calculation can be checked in Detail report as well.



Analysis Result

Plate Beam Check Result Dialog

Code : AASHTO-LRFD12 Unit : kips , in , / in
Results : Strength Serviceability

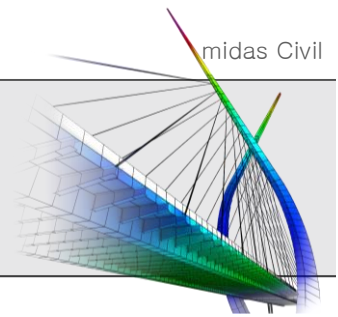
Sub-Do main	SEL	Major Dir	CHK	Pos	Use_As	Elem.	Node	LCB_M	Mu	Mr	Ratio_M	Elem.	Node	LCB_V	Vu	Vr
Top_I	<input type="checkbox"/>	Dir1	OK	Pos	0.0658	185	216	4	10.1978	21.3610	0.4774	193	4	4	0.88765	7.290
				Neg	0.0658	193	4	3	13.7431	21.3610	0.6434					
Top_I	<input type="checkbox"/>	Dir2	OK	Pos	0.0658	906	956	4	10.1978	21.3610	0.4774	771	812	4	0.88765	7.290
				Neg	0.0658	771	809	3	13.7431	21.3610	0.6434					

Design Result



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MIDAS IT Design Development Team

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*.DEFINITION OF LOAD COMBINATIONS WITH SCALING UP FACTORS.

LCB	C	Loadcase Name(Factor)	+	Loadcase Name(Factor)	+	Loadcase Name(Factor)
1	1	SW(1.250)	+	EV(1.300)	+	EH(1.350)
2	1	SW(1.250)	+	EV(1.300)	+	EH(0.900)
3	1	SW(1.500)	+	EV(1.300)	+	EH(1.350)
4	1	SW(1.500)	+	EV(1.300)	+	EH(0.900)

MIDAS/Civil - RC-Plate Beam Design [AASHTO-LRFD12] Civil 2018

*.MIDAS/Civil - RC- PLATE BEAM Analysis/Design Program.

*.PROJECT :
*.DESIGN CODE : AASHTO-LRFD12. *.UNIT SYSTEM : kips, in. /in
*.SUB-DOMAIN : Top_1 Member Type = PLATE BEAM(1D), Dir = 1)

*.DESCRIPTION OF PLATE BEAM DATA :
Thickness = 10.000 in.
Unit Width = 1 in.
Concrete Strength (fc) = 5.000 ksi.
Main Rebar Strength (fy) = 60.000 ksi.
Stirrups Strength (fys) = 60.000 ksi.
Modulus of Elasticity (Es) = 29000.000 ksi.

< Selected Elements >
All Elements
< Positive Bending Moment >
P-Mu = 0.00 in-kips/in., ELEM = 833, LCB = 1, NODE = Center
< Negative Bending Moment >
N-Mu = 28.75 in-kips/in., ELEM = 1020, LCB = 3, NODE = 1464
< Shear Force >
Vu = -0.55 kips/in. , ELEM = 863, LCB = 3, NODE = Center

*.REINFORCEMENT PATTERN :
Dt = 2.500 { in. }
Db = 2.500 { in. }

Stirrups : No BarNum

[[[+]]] ANALYZE NEGATIVE BENDING MOMENT CAPACITY.

(). Compute parameter.
-. phi = 0.90
-. Alpha = 0.85
-. Beta = 0.80
-. d = 7.5000 in.
-. ecu = 0.0030

(). Compute maximum and minimum reinforcement.
-. Rho_min1 = $(1.2) * M_{cr} / [\phi * f_y * b * d + (d-a/2)]$ = 0.0036
-. Rho_min2 = $1.33 * M_u / [\phi * f_y * b * d + (d-a/2)]$ = 0.0140
-. Rho_min = MIN(Rho_min1, Rho_min2) = 0.0036
-. As_min = Rho_min * Ag = 0.1563 in²/in.

(). Search for required reinforcement..... Unit : kips., in.

Trial	Assumed As(Top & Bottom)	Mr	Ratio	Status
1	0.0363	7.19	3.995	N.G
2	0.1785	32.97	0.872	O.K
3	0.1074	20.62	1.394	N.G
4	0.1429	26.86	1.070	N.G
5	0.1607	29.94	0.960	O.K
6	0.1518	28.41	1.012	N.G
7	0.1563	29.27	0.982	O.K
8	0.1585	29.61	0.971	O.K

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(). Check moment capacity.
-. c = 1.3906 in.
-. Cc = 4.73 kips/in.
-. Ts = 4.75 kips/in.
-. Mr = 29.61 in-kips/in.
-. Mu/Mr = 0.971 --> 0.K !

[[[+]]] ANALYZE SHEAR CAPACITY.

(). Compute shear parameter.
-. phi = 0.90
-. Av = 0.0000 in²/in.
-. bv = 1.00 in.
-. dv = 7.4648 in. (for Beta Calculation)
-. theta = 0.589 Deg.
-. Epsilon_s = MIN((Mu/dv + 0.5*Vu) / (Es*As), 0.006) = 0.0014
-. beta = 4.8 / (1+750*Epsilon_s) = 2.3817

(). Compute shear strength of concrete.
-. dv = MAX[dv, 0.9*d, 0.72*Hc] = 7.46 in.
-. Vu = -0.55 kips/in.
-. Vc = 0.0316*beta*SQRT[fc]*bv*dv = 1.26 kips/in.
-. phiVc = phi * Vc = 1.13 kips/in.
-. Vn_lim = 0.25*fc*bv*dv = 9.33 kips/in.

(). Compute stirrup spacing.
-. Maximum spacing smax = MIN(0.8*dv, 24 in) = 5.972 in.
-. Vu < phiVc/2 --> Not required shear reinforcement.
-. Applied spacing s = smax = 5.972 in.

(). Compute shear strength of reinforcement.
-. Vs = Av*fys*dv*cot(theta) / s = 0.00 kips/in.
-. Vs_lim = 0.25*fc*bv*dv - Vc = 8.07 kips/in.
-. Vs = MIN(Vs, Vs_lim) = 0.00 kips/in.
-. phiVs = phi*Vs = 0.00 kips/in.
-. phiVs > (Vu-phiVc) --> 0.K !
-. Av_req = Vs / (fys*dv*cot(theta)) = 0.0000 in²/in.

(). Check tension force in the longitudinal reinforcement caused by shear.
-. phib = 0.90
-. phiv = 0.90
-. vs1 = MIN(Vs, Vu/phiv) = 0.00 kips/in.
-. As_req = [Mu/(phib*dv) + (Vu/phiv - 0.5*vs1)*cot(theta)] / fy = 0.0249 in²/in.
-. As = 0.0101 in²/in.
-. As_req > As --> Under-reinforced !

[[[+]]] ANALYZE POSITIVE BENDING MOMENT CAPACITY.

(). Compute parameter.
-. phi = 0.90
-. Alpha = 0.85
-. Beta = 0.80
-. d = 7.5000 in.
-. ecu = 0.0030

(). Compute maximum and minimum reinforcement.
-. Rho_min1 = $(1.2) * M_{cr} / [\phi * f_y * b * d + (d-a/2)]$ = 0.0036
-. Rho_min2 = $1.33 * M_u / [\phi * f_y * b * d + (d-a/2)]$ = 0.0000
-. Rho_min = MIN(Rho_min1, Rho_min2) = 0.0036
-. As_min = Rho_min * Ag = 0.0363 in²/in.

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(). Search for required reinforcement..... Unit : kips., in.

Trial	Assumed As(Top & Bottom)	Mr	Ratio	Status
1	0.0363	7.19	0.000	O.K

(). Check moment capacity.
-. c = 0.3184 in.
-. Cc = 1.08 kips/in.
-. Ts = 1.09 kips/in.
-. Mr = 7.19 in-kips/in.
-. Mu/Mr = 0.000 --> 0.K !

Detail Result